

Identification of Parameters for Tethered Satellite System to Emulate Net-Captured Debris Towing

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- **Increasing amounts of space debris** pose threats to spacecraft operations
- Many potential systems for Active Debris Removal have been proposed (Shan et al., 2017)
 - Harpoon-Based
 - Robotic-Arms-Based
 - Net-Based
- Tether-nets are particularly promising
 - **Safe capture of large, tumbling objects**
- How can we study them?
 - **Simulation** and analysis

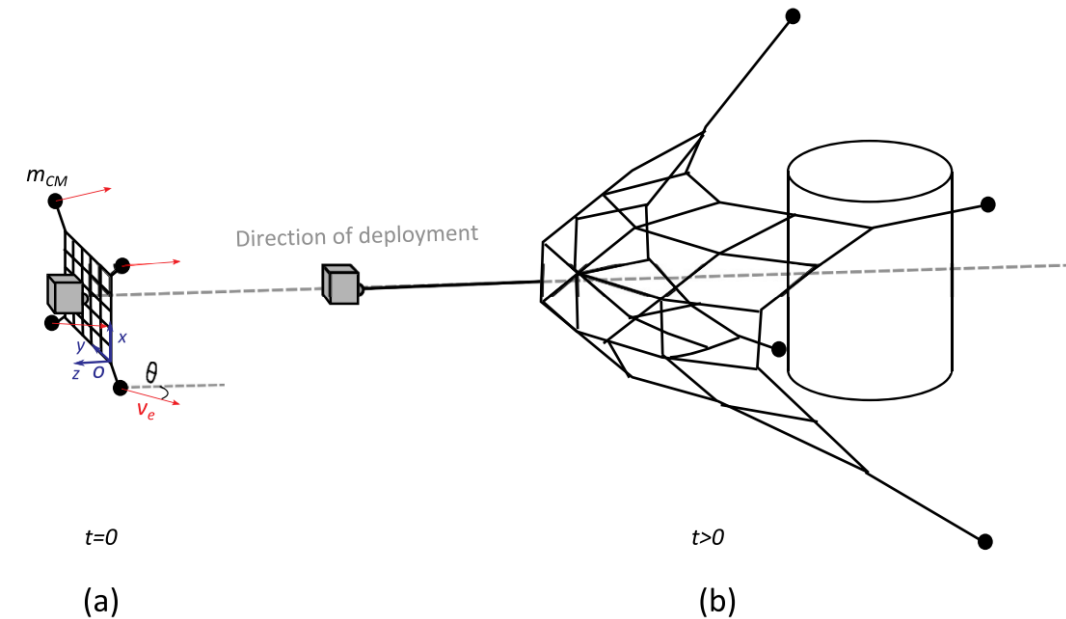
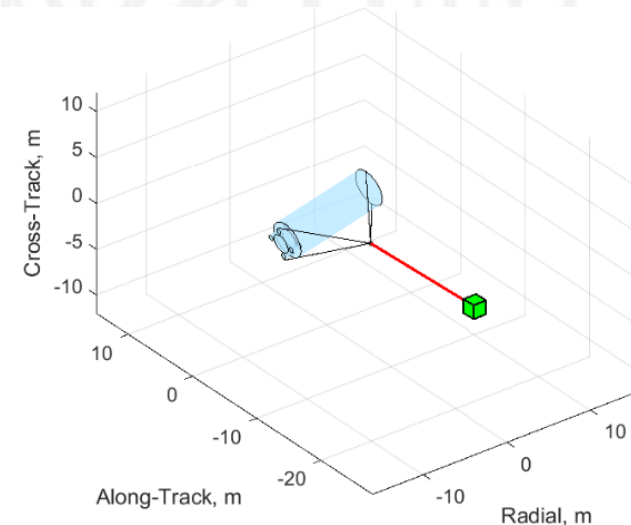
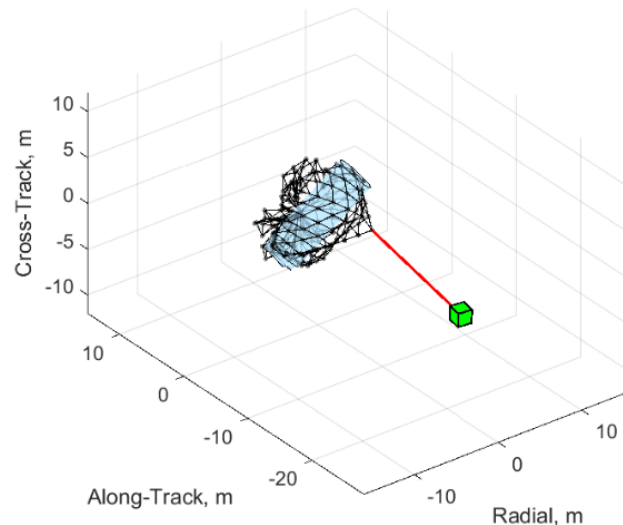


Fig. 1. Illustration of tether-net capture concept. (a): ejection. (b): configuration after deployment.

Figure from (Botta et al., 2019)

Introduction

- **Motivation:** Need a **simplified model** of the chaser-net-target system for long-duration orbital simulations.
 - High-fidelity simulations with net → **very high computational cost**
- **Model Approximation:**
 - The net is replaced with **4 tethers** rigidly connected to the target.
 - Need to **identify the appropriate properties** of the sub-tethers (STs) + tethers connection point mass of the lower-order model that **best represent** the high-fidelity dynamics.





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Net Capture System and Target Debris

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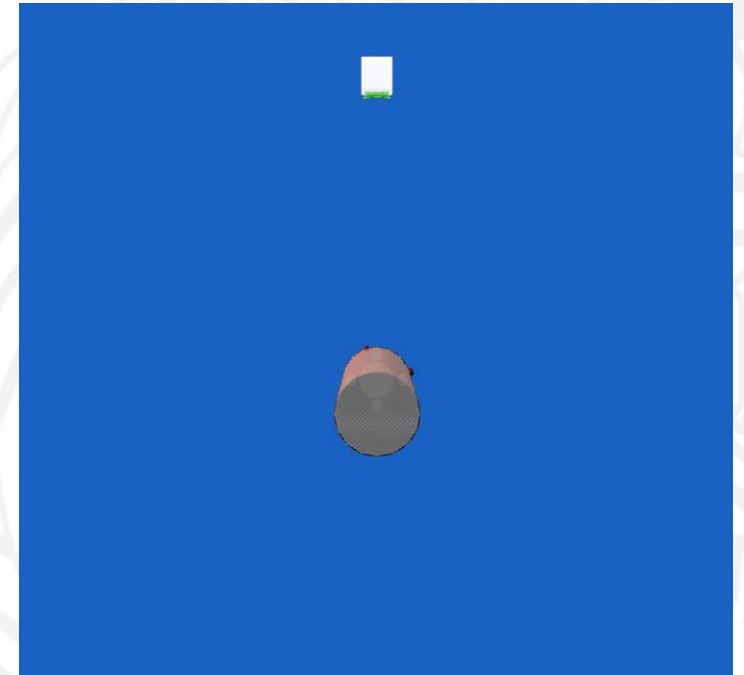
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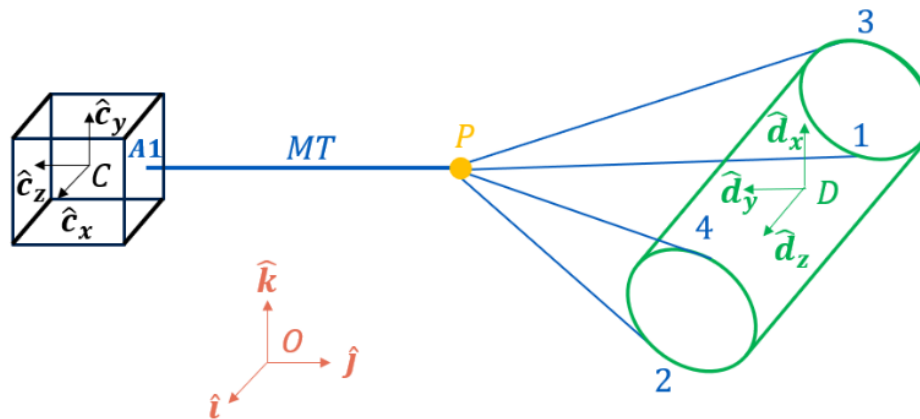
- Net modeled via the **lumped-parameter modeling method**
 - **Computational challenge:** The entire system often involves **1000+ degrees of freedom**
- **Corner masses** used to guide the net to the target.
- Net includes a **closing mechanism**, attached to the chaser by the **main tether (MT) and winch**.
- Sliding-mode **attitude controller** present on the cubic chaser to maintain desired orientation.
- **Target debris:** Zenit-2 rocket upper stage

Net simulator detailed within (Botta et al., 2019)



Sub-Tether Tethered Satellite System

- Chaser and debris are **rigid bodies** with the same dimensions as with the high-fidelity model.
- All tethers modeled as nonlinear spring-damper (**Kelvin–Voigt**) elements.
 - MT is given the **same length, stiffness, and damping properties** as with the high-fidelity model.
- Connection point P links the **MT to the 4 STs**.
 - Modeled as a point mass
- Sliding-mode **attitude controller** present on the cubic chaser to maintain desired orientation.



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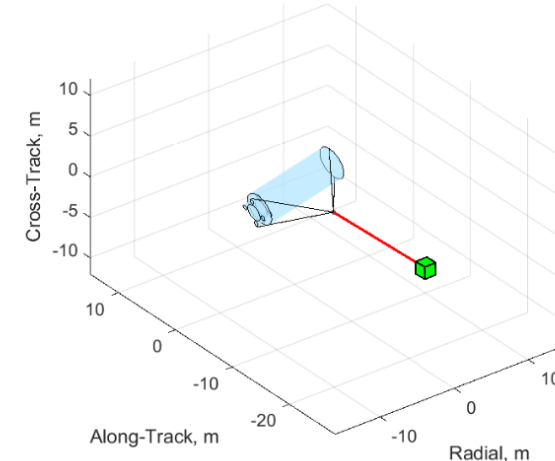
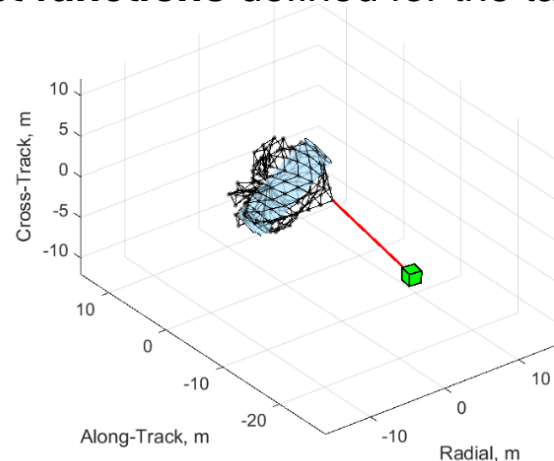
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Parameter Identification

- **Parameter Identification Process:**
 - Perform **6 high-fidelity** debris towing simulations
 - **3 for parameter identification** via solving optimization problems.
 - **3 for validation** of the parameters on unseen data.
 - Use all same initial conditions, except for **initial target angular velocity**.
 - Perform **optimization** to determine the lower-order model parameters which **minimize dynamics difference** with the high-fidelity model.
 - **2 cost functions** defined for the task



Cost Functions

$(.)^{\mathcal{H}}$: High-fidelity model quantities
 $(.)^{\mathcal{L}}$: Lower-order model quantities

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- Cost Function 1:** Difference in (i) chaser-debris relative position, (ii) debris angular velocity, and (iii) chaser angular velocity between models.

$$\begin{aligned}
 \mathbf{r}_{D/C}^{\mathcal{H}} &= \mathbf{r}_{D/O}^{\mathcal{H}} - \mathbf{r}_{C/O}^{\mathcal{H}} & f_1(s) &= \sum_{j=1}^3 w_1 \text{RMSE}_{r,j} + \\
 \mathbf{r}_{D/C}^{\mathcal{L}} &= \mathbf{r}_{D/O}^{\mathcal{L}} - \mathbf{r}_{C/O}^{\mathcal{L}} & & w_2 (\text{RMSE}_{\omega_D,j} + \text{RMSE}_{\omega_C,j}) \\
 \mathbf{r}_{\Delta} &= \mathbf{r}_{D/C}^{\mathcal{L}} - \mathbf{r}_{D/C}^{\mathcal{H}}
 \end{aligned}$$

$$\begin{aligned}
 \boldsymbol{\omega}_{C,\Delta} &= (\boldsymbol{\omega}^C)^{\mathcal{L}} - (\boldsymbol{\omega}^C)^{\mathcal{H}} \\
 \boldsymbol{\omega}_{D,\Delta} &= (\boldsymbol{\omega}^D)^{\mathcal{L}} - (\boldsymbol{\omega}^D)^{\mathcal{H}} \\
 \text{RMSE}_{r,j} &= \sqrt{\sum_{g=1}^N \frac{\|\mathbf{r}_{\Delta,j,g}\|^2}{N}}
 \end{aligned}$$

$$\text{RMSE}_{\omega_D,j} = \sqrt{\sum_{g=1}^N \frac{\|\boldsymbol{\omega}_{D,\Delta,j,g}\|^2}{N}}$$

$$\text{RMSE}_{\omega_C,j} = \sqrt{\sum_{g=1}^N \frac{\|\boldsymbol{\omega}_{C,\Delta,j,g}\|^2}{N}}$$

- Cost Function 2:** Difference in the MT tension between models.

- MT tensions **dependent on the relative dynamics** → may indirectly enable the relative dynamics to be as identical as possible.

$$f_2(s) = \sum_{j=1}^3 \text{RMSE}_{T,j}$$

$$\text{RMSE}_{T,j} = \sqrt{\sum_{g=1}^N \frac{(T_j^{\mathcal{H}} - T_j^{\mathcal{L}})^2}{N}}$$

Optimization Problem Formulation

$$\min_{\mathbf{s}} f_k(\mathbf{s})$$

where: $\mathbf{s} = [s_1, s_2, s_3, s_4], k = 1, 2$

$$s_{j, LB} \leq s_j \leq s_{j, UB}$$

Chosen Solver →

- **Notes:**

- Do not know the shapes of the cost functions
 - Likely ***nonconvex*** with respect to the design variables
 - ***Gradients unknown***
- Nonlinear programming problem
- No constraints given on the value of the cost functions
 - Only upper and lower bounds given to design variables

- **Mesh Adaptive Direct Search (MADS)**
 - Derivative-free optimization solver
 - Utilized in many scientific and engineering application
 - (Alarie et al., 2021)
 - Requires an initial guess to be given

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Converged Optimization Results

- **Converged design variables differ** based on the choice of initial guesses.
 - **More drastic change using Cost Function 2** compared to 1 for different initial guess.

Converged Cost Function Values for Training Dataset

Obj. Function	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
$f_1(s)$	10.3854	10.3915	10.3824	10.3853	10.3859
$f_2(s)$	272.03	292.99	292.46	272.15	292.818

Converged Decision Variables Using $f_1(s)$

Variables	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
s_1	1.3942	1.3932	1.3948	1.3943	1.3943
s_2	6.5288	6.5180	6.5406	6.5281	6.5282
s_3	1.3114	1.3058	1.3257	1.3145	1.3131
s_4	0.5602	0.7534	0.2726	0.5546	0.5832

Converged Decision Variables Using $f_2(s)$

Variables	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
s_1	2.7398	1.0409	2.5097	2.7454	1.1012
s_2	8.5805	9.1683	6.5366	8.6522	9.1923
s_3	2.1721	2.8961	2.3678	2.1952	2.8975
s_4	1.0000	0.5933	0.3817	0.1608	0.1371

Best Converge Cost Function 1 value and design variables

Best Converge Cost Function 2 value and design variables

Converged Optimization Results

- Converged design variables differ** based on the choice of initial guesses.
 - More drastic change using Cost Function 2** compared to 1 for different initial guess.
- Evaluating **cost functions using validation dataset + converged design variables** yielded similar costs.

Cost Function Values for Validation Dataset

Obj. Function	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
$f_1(s)$	11.8821	11.8982	11.8601	11.8814	11.8826
$f_2(s)$	293.37	287.97	326.78	290.73	288.55

Converged Decision Variables Using $f_1(s)$

Best Converge Cost Function 1 value and design variables

Variables	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
s_1	1.3942	1.3932	1.3948	1.3943	1.3943
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Converged Decision Variables Using $f_2(s)$

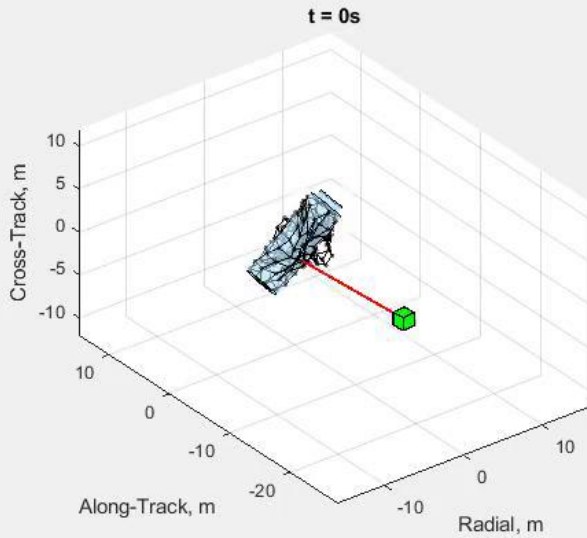
Best Converge Cost Function 2 value and design variables

Variables	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
s_1	2.7398	1.0409	2.5097	2.7454	1.1012
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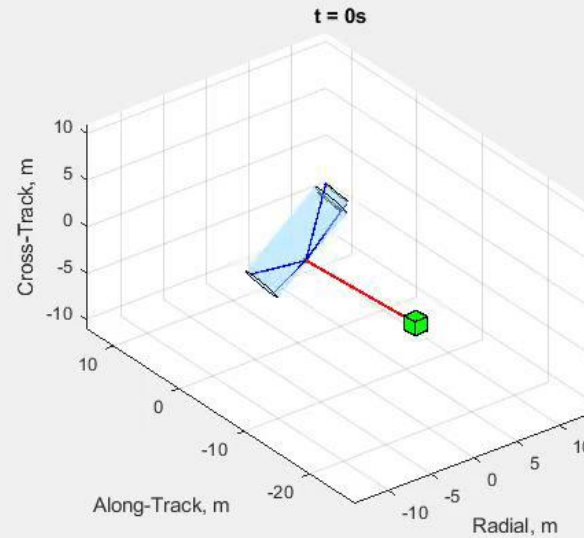
Sample Scenario Comparison

- Overall **dynamics similar** between the models
 - Chaser attitude in the high-fidelity model **less stabilized** than in the lower-order simulations

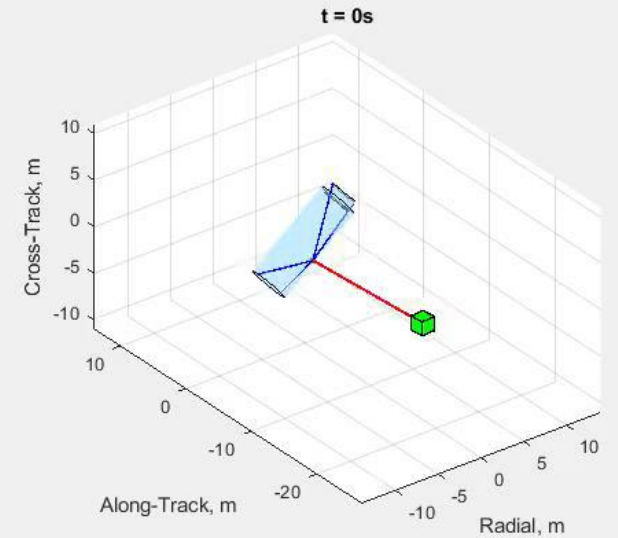
High-Fidelity Full-Net System



ST System With Parameters Obtained From Best Cost Function 1 Optimization



ST System With Parameters Obtained From Best Cost Function 2 Optimization



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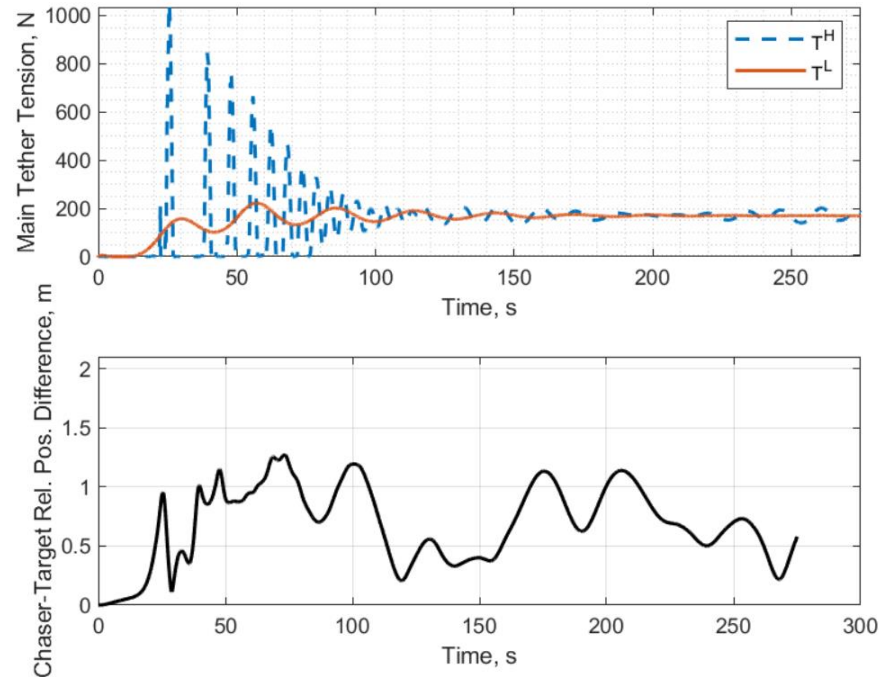
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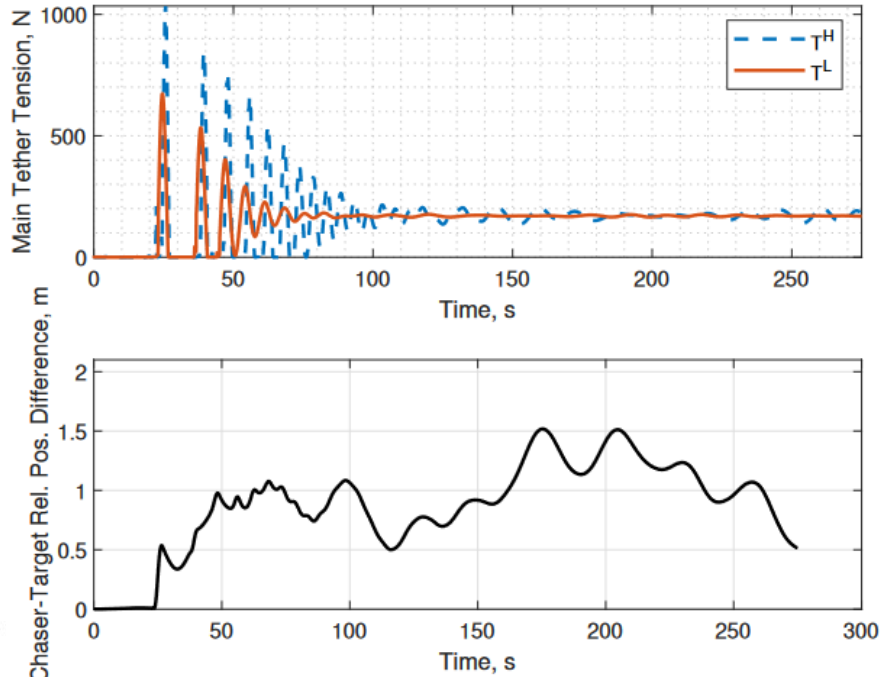
Sample Scenario Comparison

- Overall **dynamics similar** between the models
 - Parameters from Cost Function 1 results in ***better relative dynamics matching***; Cost Function 2 results in ***better MT tension matching***.

High vs. Low Fidelity: ST System With Parameters Obtained From Best Cost Function 1 Optimization



High vs. Low Fidelity: ST System With Parameters Obtained From Best Cost Function 2 Optimization



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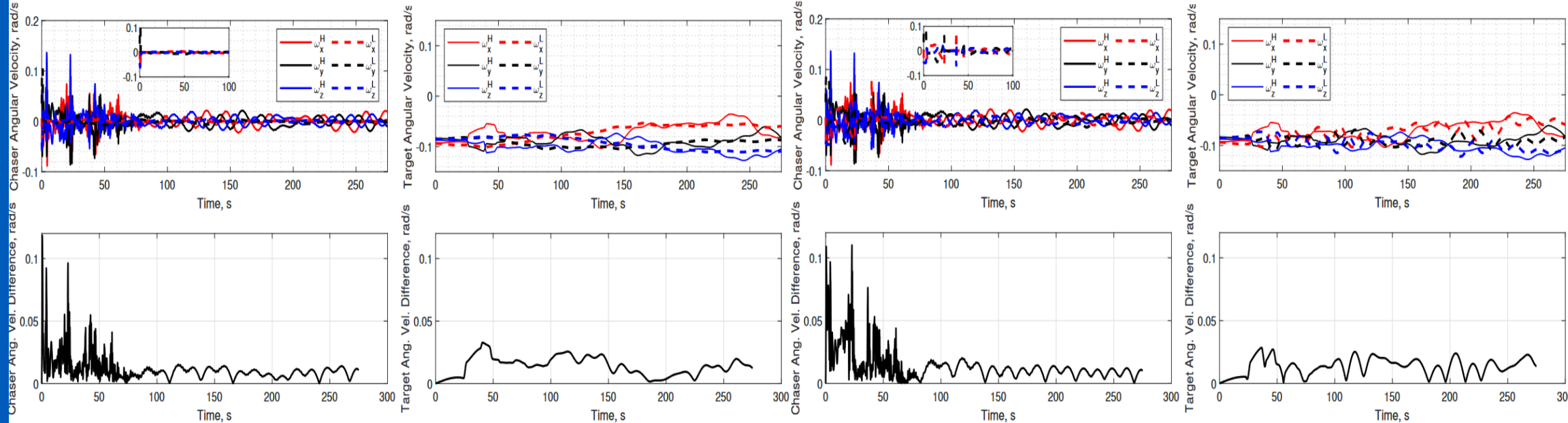
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Sample Scenario Comparison

- Overall **dynamics similar** between the models
 - High-fidelity **chaser attitude dynamics is less stabilized** compared to both lower-order simulations.
 - Using parameters from Cost Function 1 results in **better debris angular rates matching**.

**High vs. Low Fidelity: ST System With Parameters
 Obtained From Best Cost Function 1 Optimization**

**High vs. Low Fidelity: ST System With Parameters
 Obtained From Best Cost Function 2 Optimization**



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Conclusion

- **Parameter identification framework** proposed to allow lower-order TSS model to best approx. net-based debris towing.
- **Two optimization cost functions** were formulated to **minimize the difference in dynamics quantities** of interest between models.
 - Lower-order TSS with determined parameters demonstrated ***satisfactory dynamics matching performance***.
- Compared to Cost Function 2, Cost Function 1 demonstrated:
 - **Less sensitivity to initial guesses**
 - **Better overall dynamics matching** (except MT tension).
- **Future work:** Apply the framework to larger datasets with **larger variations** in the simulation's initial conditions.

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References

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Thank you!

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Systems Parameters and Initial Conditions

System Parameters For Both High-Fidelity and Lower-Order Simulations

Variables	Value	Units
Chaser Mass, m_C	1600	kg
Nominal Debris Mass, m_D	9000	kg
Chaser Side Length, L_C	1.5	m
Debris Length, L_D	11	m
Debris Diameter, d_D	3.9	m
Chaser Inertia Matrix, J_C	diag(266.67, 266.67, 266.67)	kgm ²
Debris Inertia Matrix, J_D	diag(94880, 94880, 46295.5)	kgm ²
Chaser Attachment Point, $[\mathbf{r}_{A1/C}]_C$	$[0, 0, -0.75]^T$	m
Debris Attachment Point 1, $[\mathbf{r}_{1/D}]_D$	$[-1.9500, 0, -5.7170]^T$	m
Debris Attachment Point 2, $[\mathbf{r}_{2/D}]_D$	$[-1.9500, 0, 5.2830]^T$	m
Debris Attachment Point 3, $[\mathbf{r}_{3/D}]_D$	$[1.9500, 0, -5.7170]^T$	m
Debris Attachment Point 4, $[\mathbf{r}_{4/D}]_D$	$[1.9500, 0, 5.2830]^T$	m
Main-tether Stiffness, k_{MT}	3000	N/m
Main-tether Damping, c_{MT}	300	Ns/m
Main-tether Natural Length, l_{MT}	15.0	m
Time for chaser thrust to reach maximum, t_{slope}	50	s

Initial Conditions For the High Fidelity Simulations

Variables	Value	Units
$\mathbf{r}_{C/O}$	$[4.95199, -1.0547469, -4.65022589]^T \times 10^6$	m
${}^O\mathbf{v}_{C/O}$	$[4.771333506, 4.267936104, 4.119936176]^T \times 10^3$	m/s
\mathbf{q}_C	$[0.506372, 0.628113, -0.5865386, -0.0709467]^T$	-
${}^O\boldsymbol{\omega}^C$	$[-0.0085526588, 0.019837, 0.0020484]^T$	rad/s
$\mathbf{r}_{D/O}$	$[4.952002, -1.054735, -4.650215]^T \times 10^6$	m
${}^O\mathbf{v}_{D/O}$	$[4.771338, 4.267935, 4.1199337]^T \times 10^3$	m/s
\mathbf{q}_D	$[0.3834407, 0.4526303, 0.7957778, 0.12180569]^T$	-
${}^O\boldsymbol{\omega}^D$	$ {}^O\boldsymbol{\omega}^D(0) \cdot [0.0047695, -0.9999851, 0.002652839]^T$	rad/s
$\mathbf{r}_{P/O}$	$[4.951991, -1.05474644, -4.6502254]^T \times 10^6$	m
${}^O\mathbf{v}_{P/O}$	$[4.771333506, 4.267936104, 4.119936176]^T \times 10^3$	m/s

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Converged Optimization Results

- Provided Initial Guess

List of Initial Decision Variables Given to The Optimization Solver

Variables	Initial Guess 1	Initial Guess 2	Initial Guess 3	Initial Guess 4	Initial Guess 5
s_1	3	2	3	3	3
s_2	9	9	8	9	9
s_3	1	1	1	2	1
s_4	0.5	0.5	0.5	0.5	0.75

- Best converged design variables are converted and displayed as physical parameters below:

Parameter	$f_1(s)$	$f_2(s)$
$k_{ST}, \text{N/m}$	24.819	549.28
l_{ST}, m	6.5406	8.5805
$c_{ST}, \text{Ns/m}$	21.169	148.627
m_p, kg	0.7449	2.7326

- Initial Debris Angular Speed for different simulations:

Simulation #	$\ \omega^D(0)\ $
1	0.16654 rad/s
2	0.16151 rad/s
3	0.15985 rad/s
4	0.15301 rad/s
5	0.14948 rad/s
6	0.14622 rad/s