

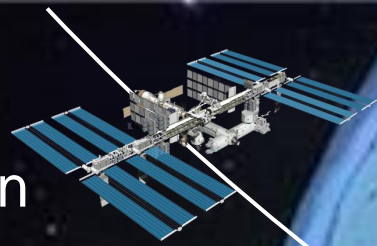
Bare Photovoltaic Tether Characteristics for ISS reboost

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Anese Giovanni

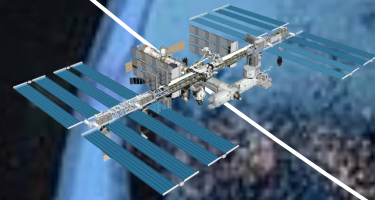
Ph.D. Student at CISAS “G.Colombo”
University of Padova

1. International Space Station



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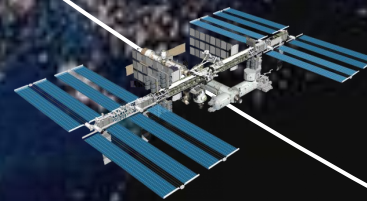
2. Bare Photovoltaic Tethers



1. International Space Station

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3. Zig-zag reboost strategy

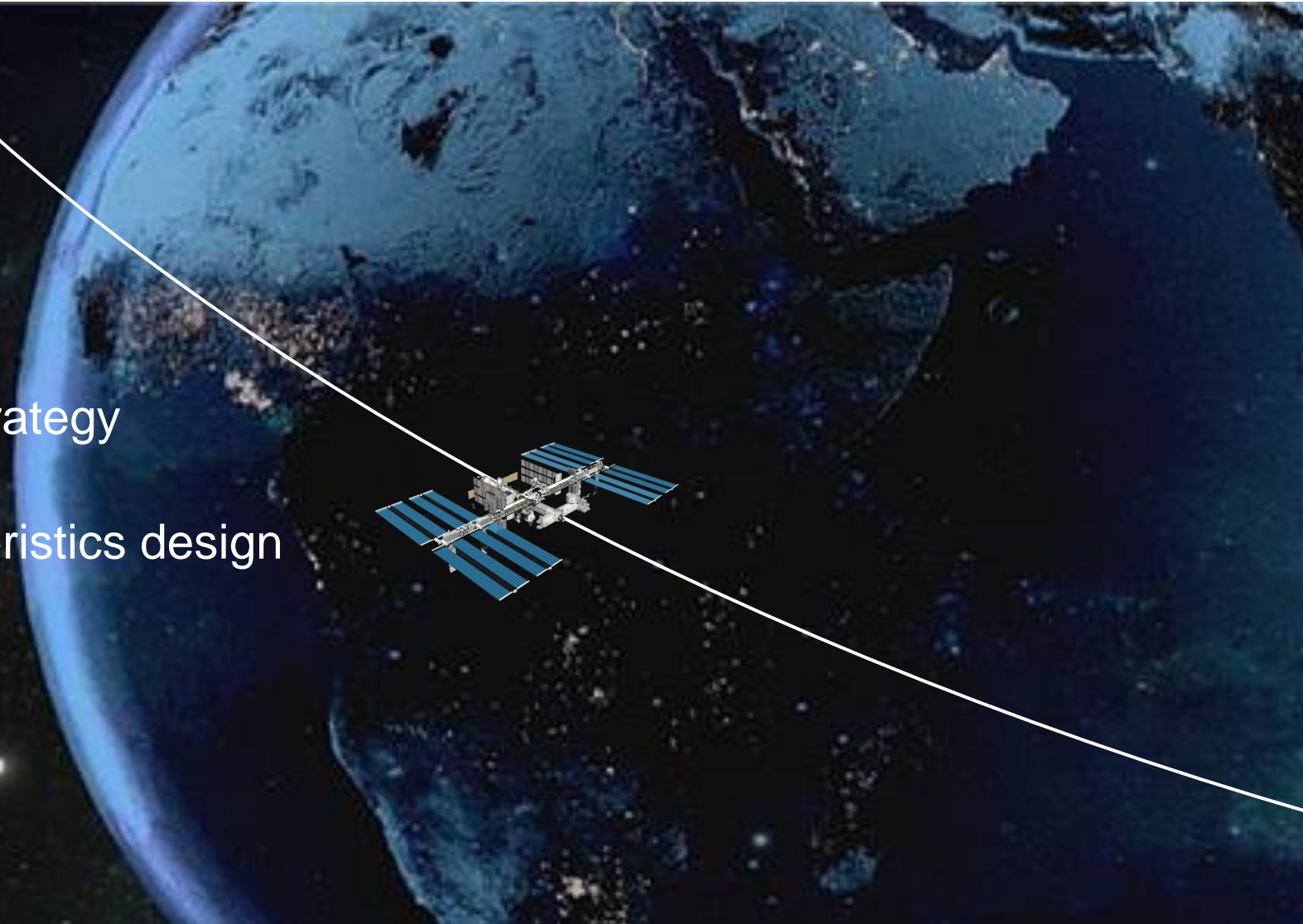


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4. Tether characteristics design



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5. Simulations and results

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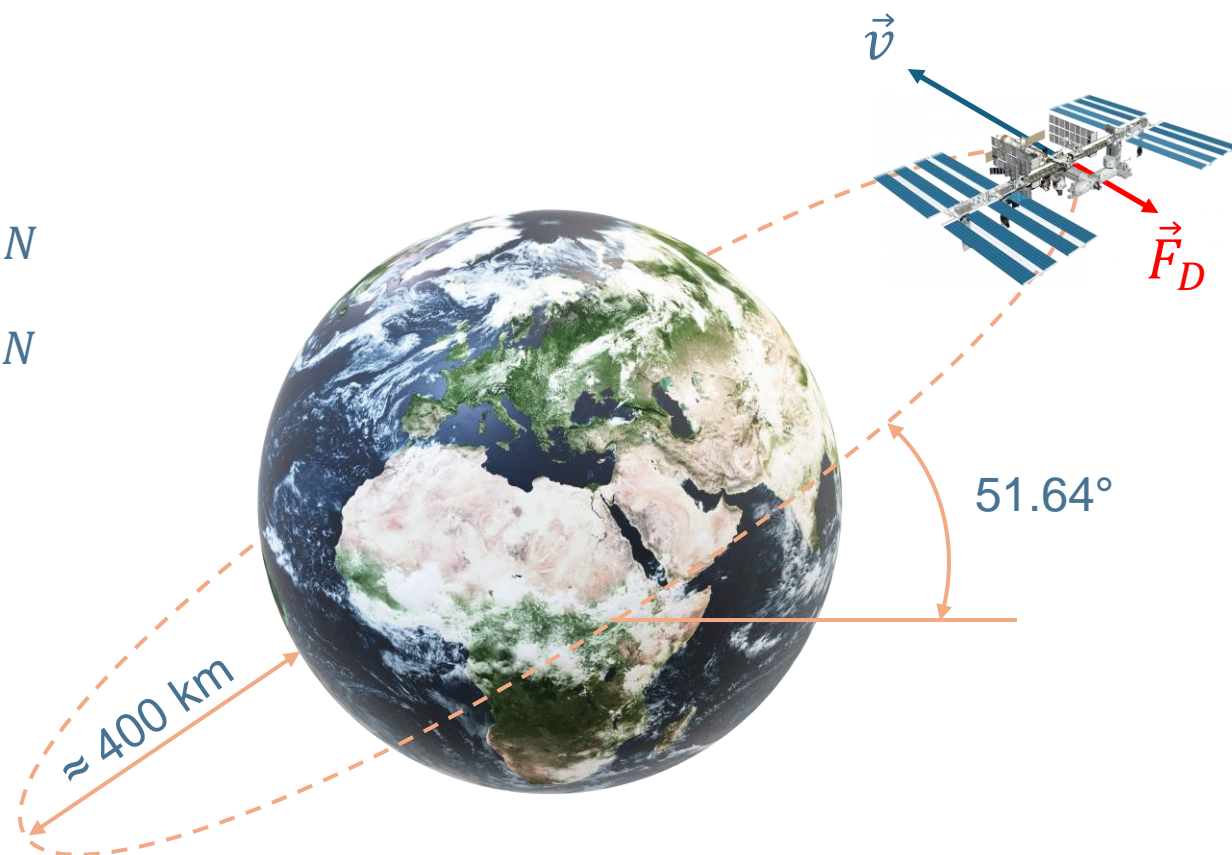
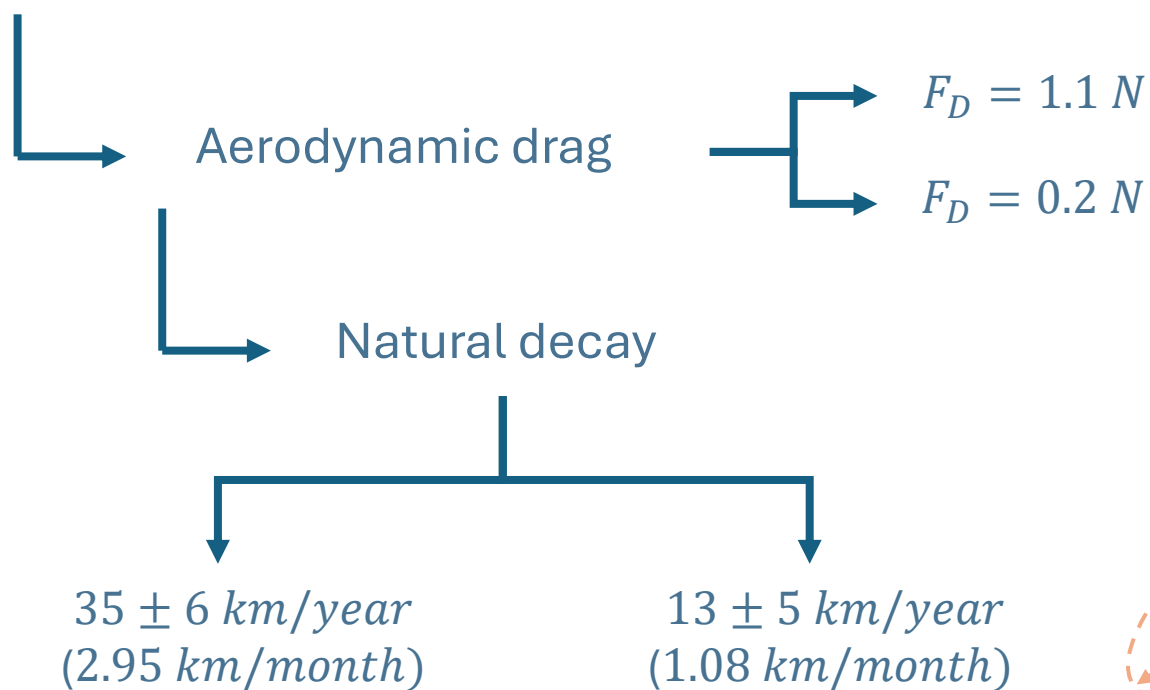
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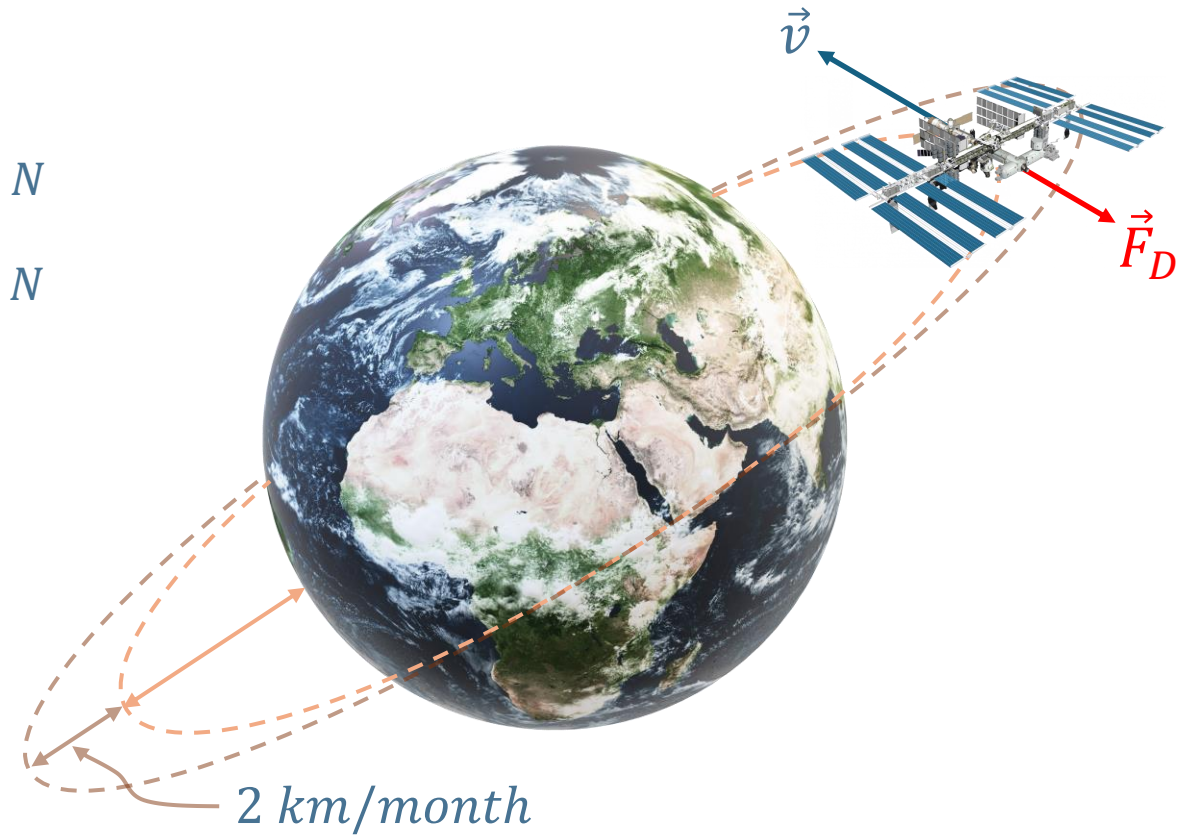
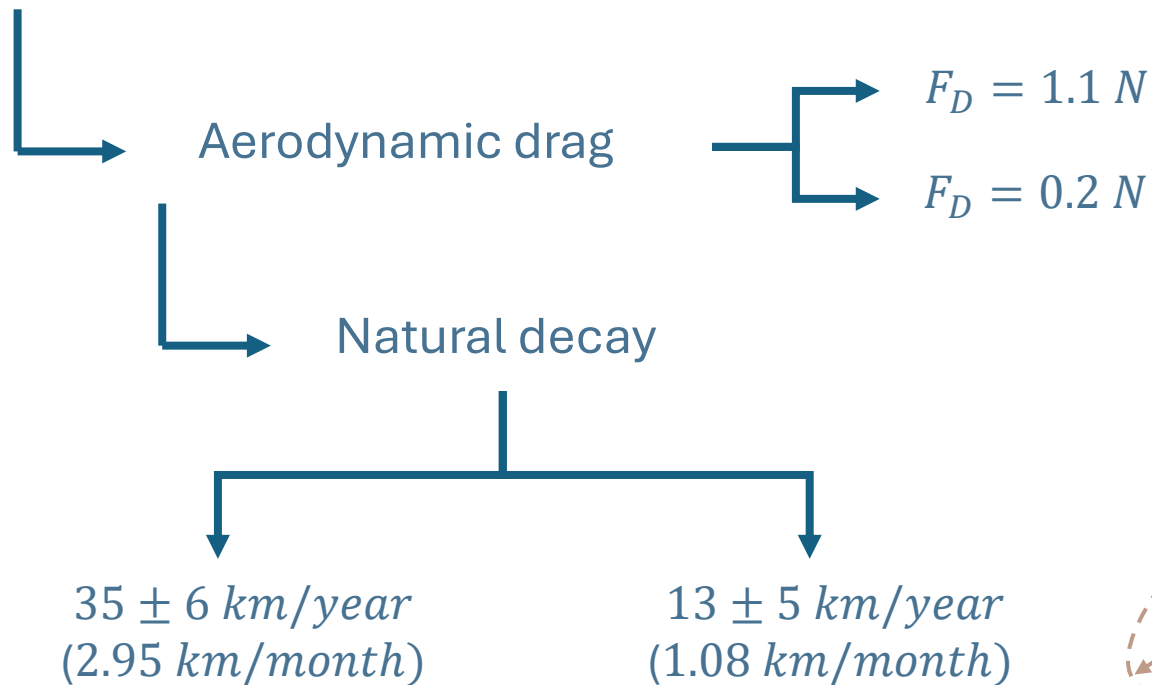
5. Simulations and results

6. Conclusions

- Orbit inclination of $\approx 51.64^\circ$
- Low Earth Orbit (LEO), altitude of $\approx 400 \text{ km}$

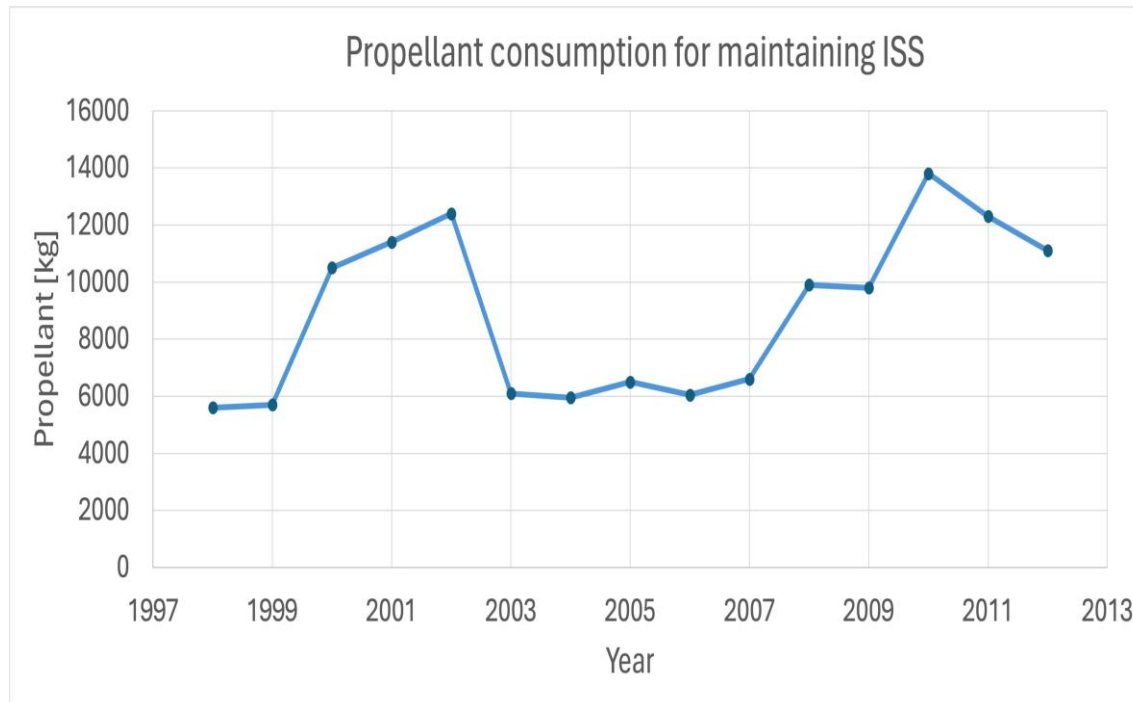
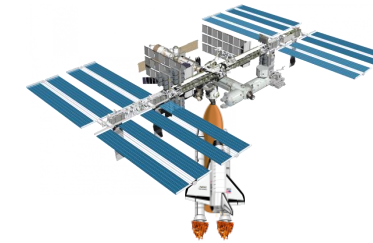


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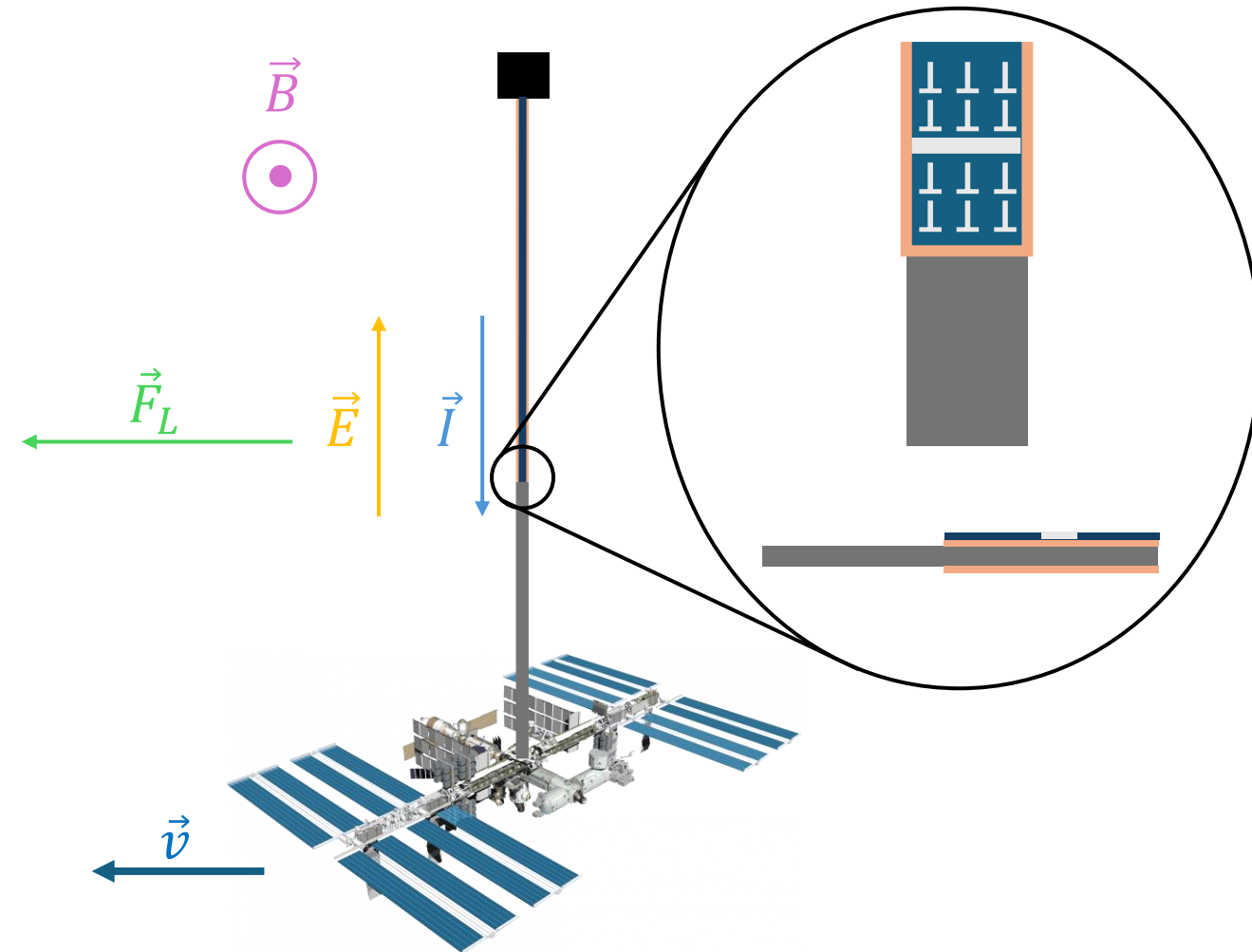


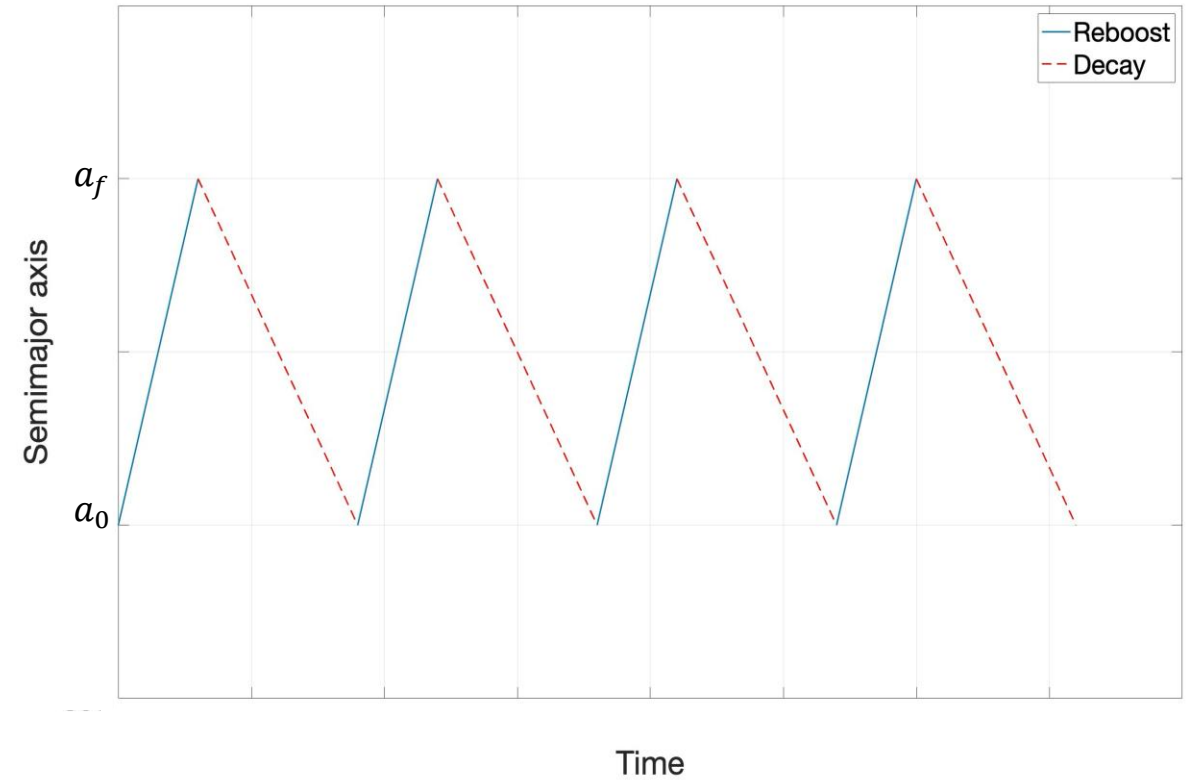
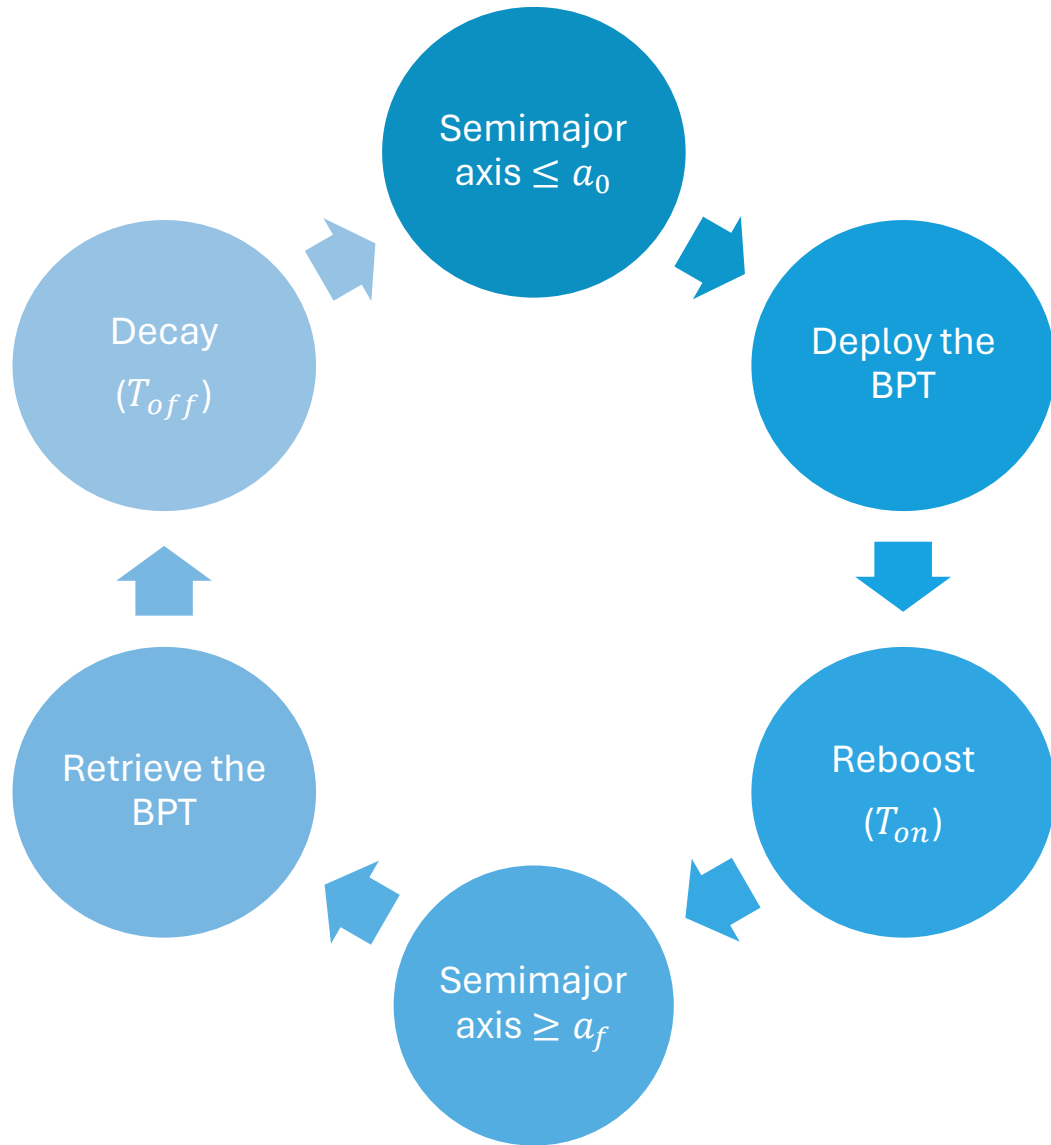
Reboost maneuvers are required periodically.

Several tons of propellant are used.



- Electro dynamic tether (EDT) architecture
- Thin film of solar cells
- Solar cells harvest power when illuminated by solar rays
 - Fully autonomous system
- Upward deployment
 - Satisfies the $\mathbf{E} \cdot \mathbf{I} < 0$ condition (active mode)
 - Avoids the approaching corridors





$$\dot{\mathbf{r}} = -\frac{\mu}{r^3} \mathbf{r} + \frac{\mathbf{F}}{m_{ISS}}$$

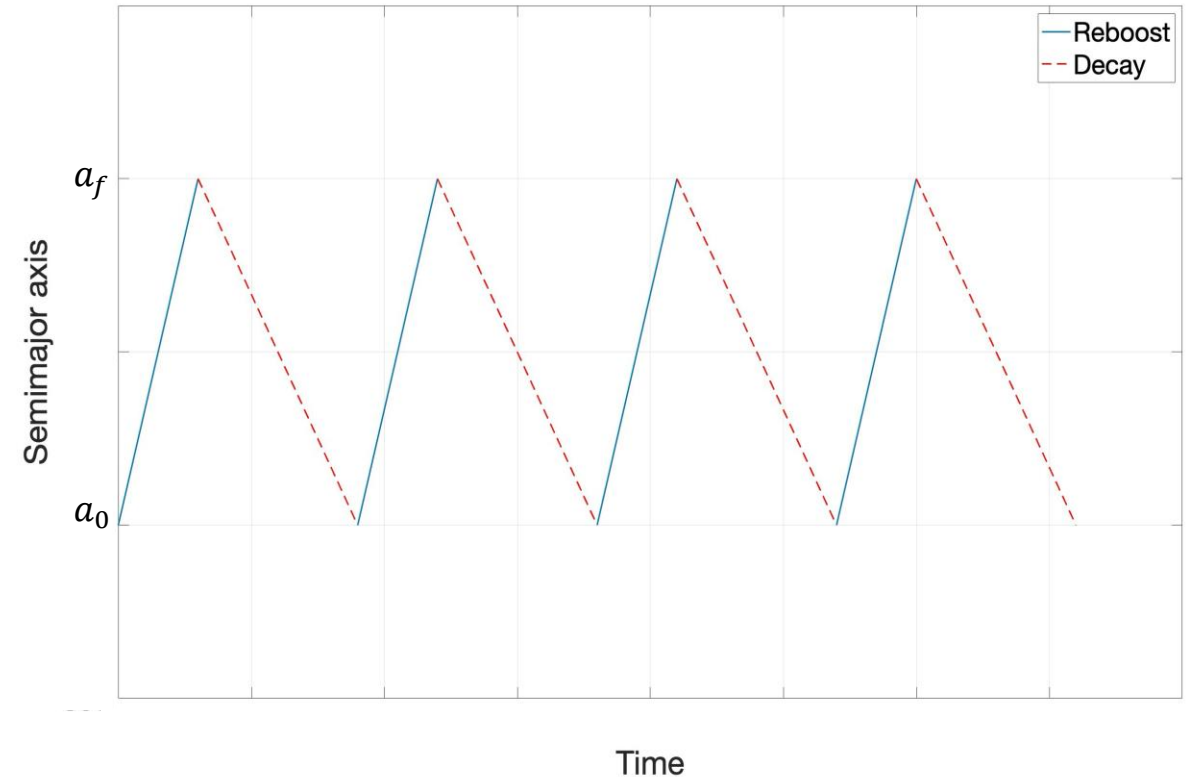
- Small eccentricity
- F_D, F_L and v are assumed not varying with a

$$T_{on} - \frac{\mu m_{ISS}}{2(F_L - F_D) \cdot v} \frac{a_f - a_0}{a_0 a_f} = 0$$

$$\tau_{on} - \frac{1}{2(\xi_t i_{av} - \tilde{W}_D)} \frac{a_f - a_0}{a_f} = 0$$

Goal: find η_{pv} for different tether geometries (L_{bare}, L_{pv}) and aerodynamic drag forces.

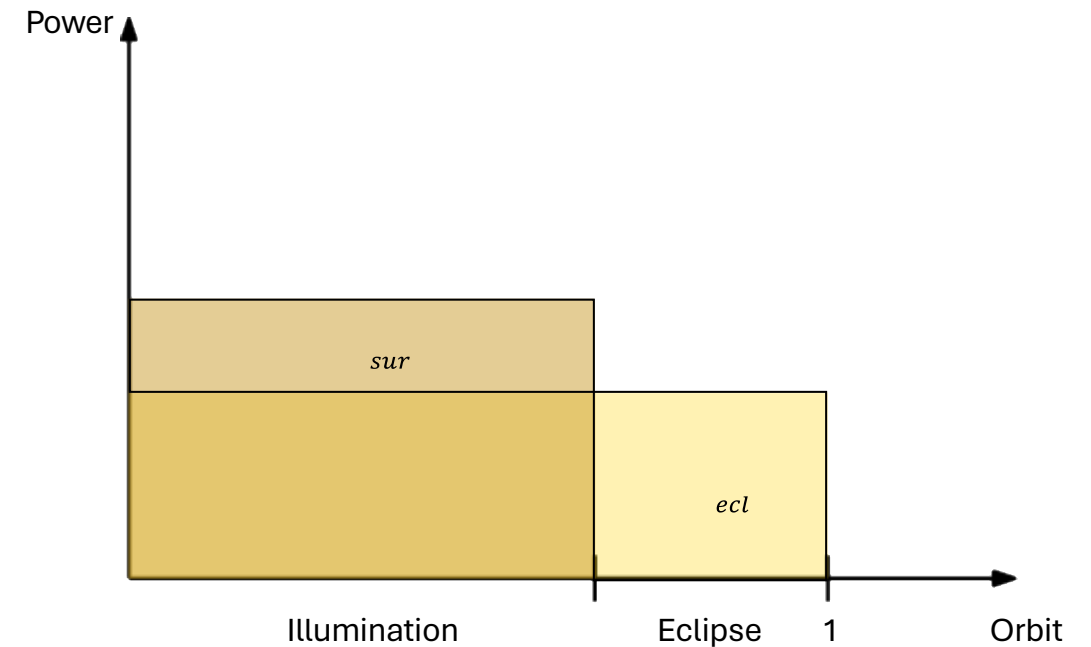
$$\eta_{pv,k+1} = \eta_{pv,k} - \frac{g(\eta_{pv,k})}{g'(\eta_{pv,k})}$$



During solar illumination a higher power must be harvested by the cells.

Higher cells efficiency and batteries to store the power are required.

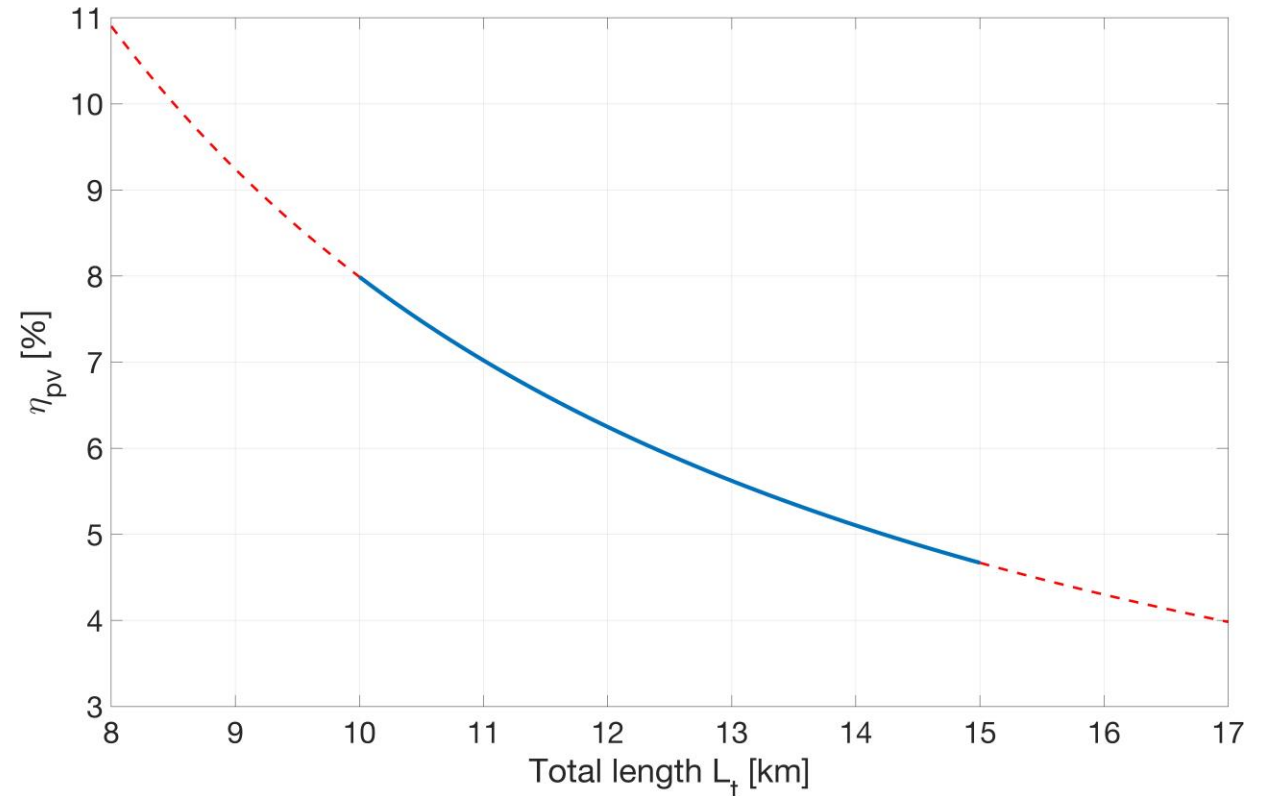
$$f_{ecl} = \frac{W_{orbit}}{W_{illumination}} = \frac{t_{orbit}}{t_{illumination}}$$



Parameters	Value
m_{ISS}	450000 <i>kg</i>
A_{ISS}	1670 m^2
C_D	2.2
w_t	50 <i>mm</i>
t_t	50 μm
σ_t	$3.55 \cdot 10^7 (\Omega m)^{-1}$
V_C	-30 <i>V</i>
E_m	0.12 <i>V/m</i>
N_0	$5.90 \cdot 10^{11} m^{-3}$
T_{on}	30 <i>days</i>
F_D	0.4 ÷ 0.8 <i>N</i>
a_0	400 <i>km</i>
a_f	404 <i>km</i>

L_t [km]	f_i [%]	L_{pv} [km]	η_{pv} [%]
10.00	90	9.00	7.99
10.50	90	9.45	7.48
11.00	90	9.90	7.02
11.50	90	10.35	6.61
12.00	90	10.80	6.25
12.50	90	11.25	5.92
13.00	90	11.70	5.62
13.50	90	12.15	5.35
14.00	90	12.60	5.10
14.50	90	13.05	4.88
15.00	90	13.50	4.67

$$F_D = 0.4 N$$

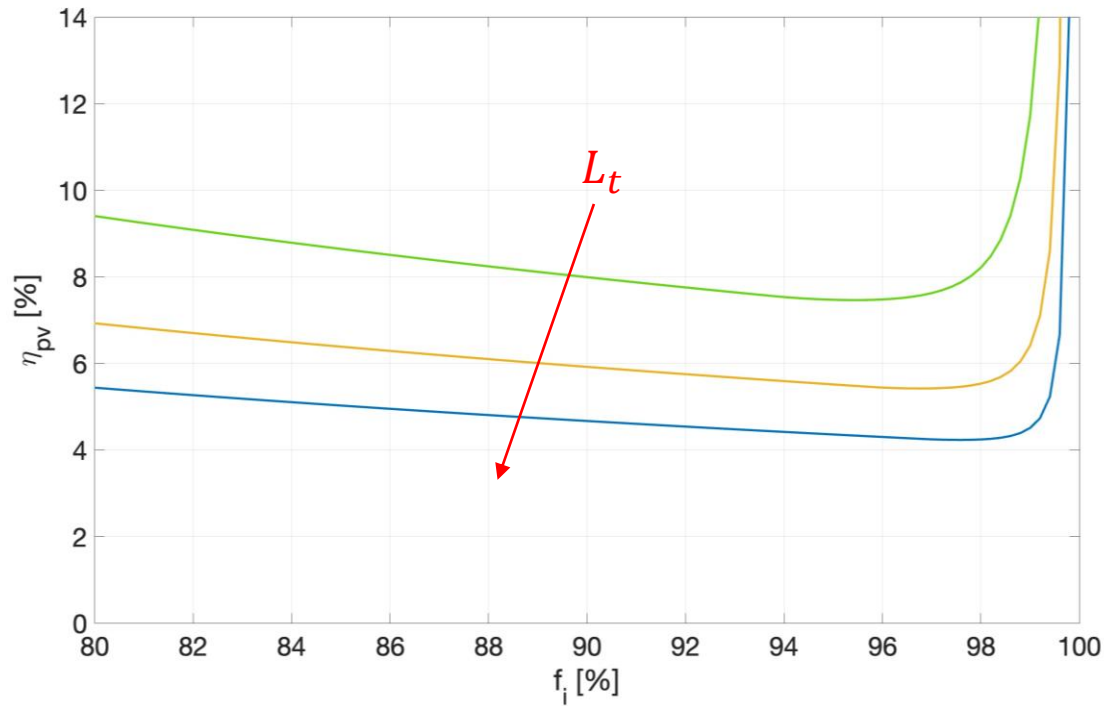


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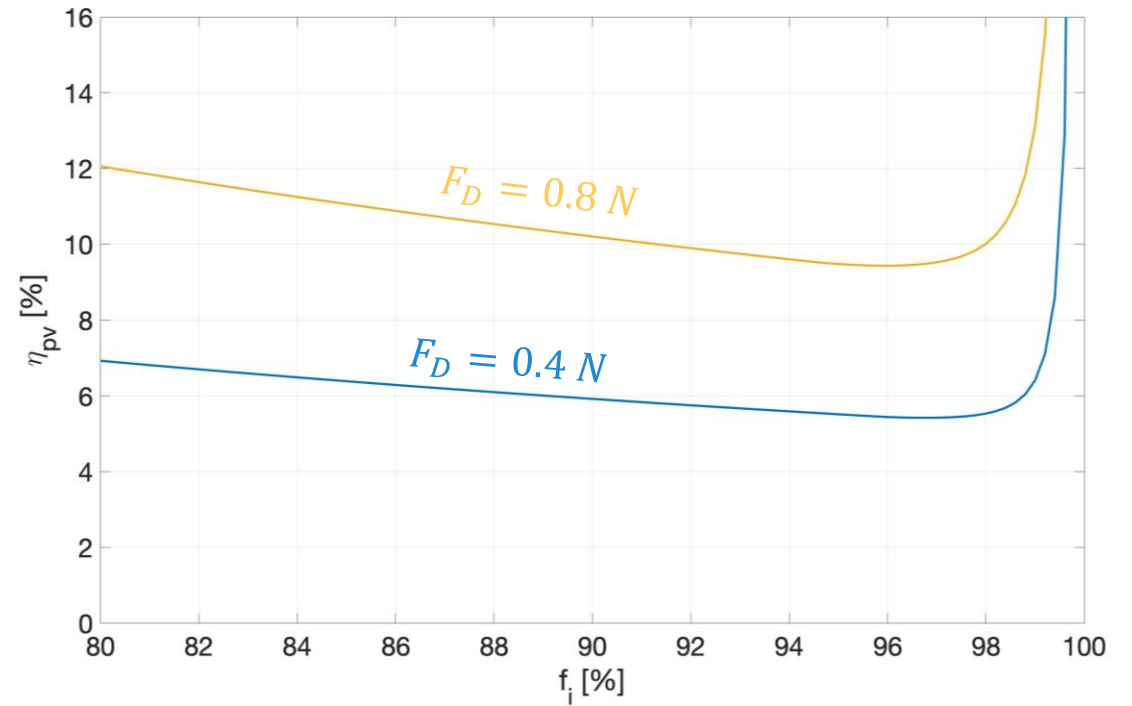
$$F_D = 0.4 N$$

L_t [km]	f_i [%]	L_{pv} [km]	η_{pv} [%]
10.00	90	9.00	14.04
10.50	90	9.45	12.23
11.00	90	9.90	10.81
11.50	90	10.35	9.66
12.00	90	10.80	8.72
12.50	90	11.25	7.93
13.00	90	11.70	7.27
13.50	90	12.15	6.70
14.00	90	12.60	6.21
14.50	90	13.05	5.78
15.00	90	13.50	5.41

$$F_D = 0.8 N$$



$F_D = 0.4 N$
 $L_t = 10, 12.5, 15 km$



$F_D = 0.4 \text{ and } 0.8 N$
 $L_t = 12.5 km$

Outputs from previous analysis must be validated. Thus they are used as inputs for simulations performed using **FLEXSIM**.

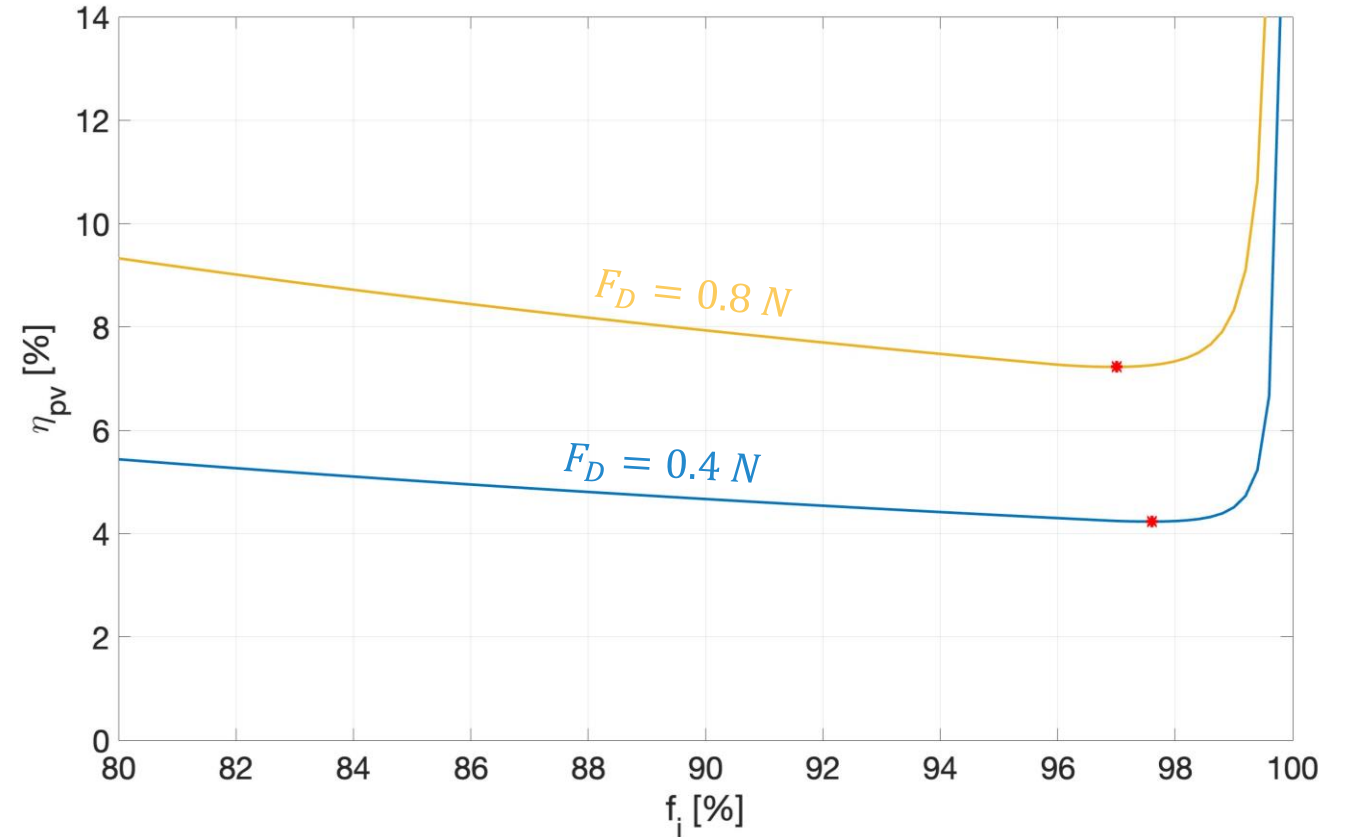
- a software fully developed at the University of Padua for the E.T.PACK project initiative.
- allows to simulate both deorbiting and reboost missions with electrodynamic and bare photovoltaic tethers.

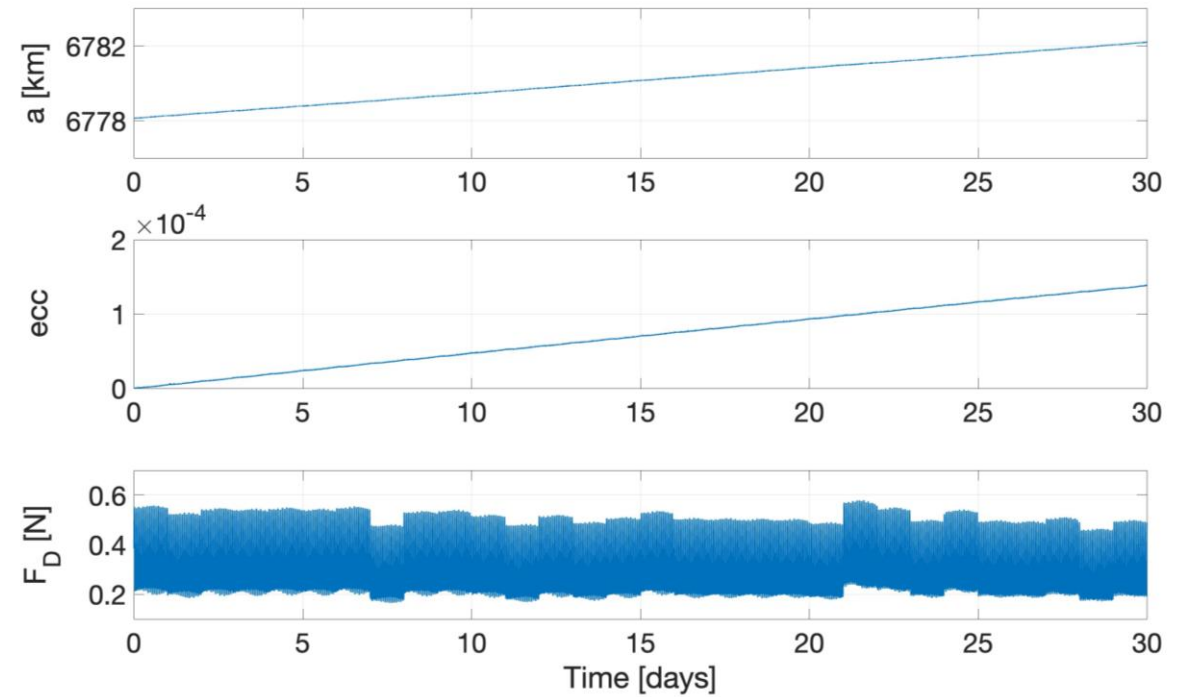
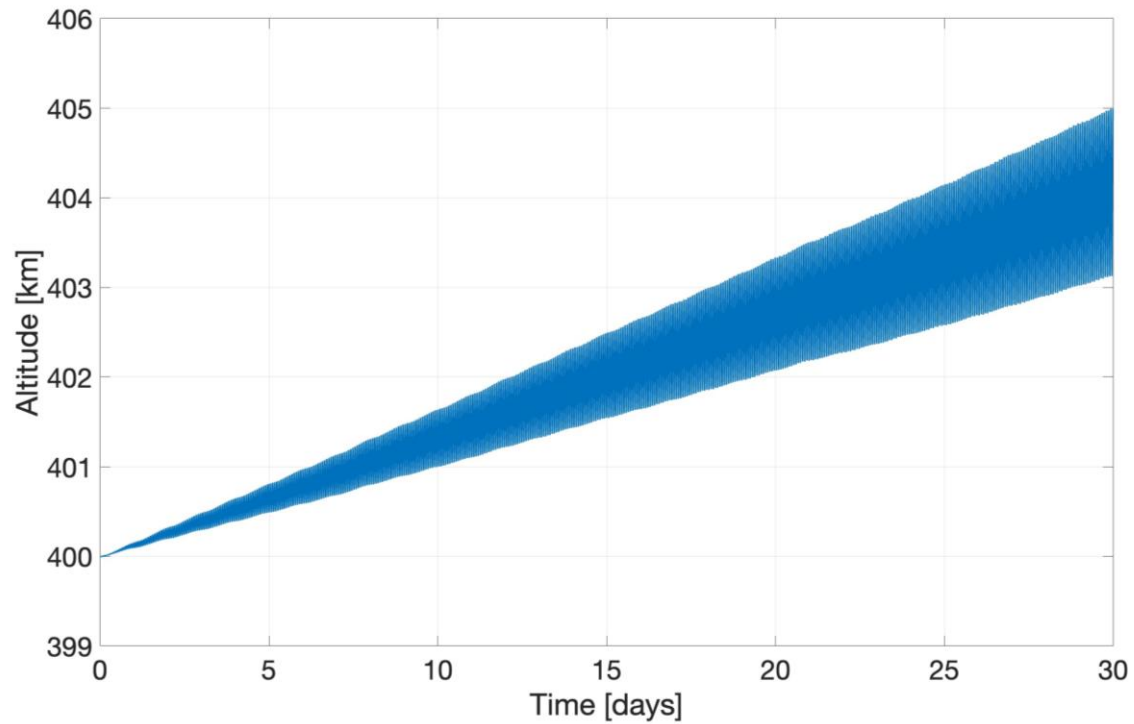
Models adopted:

- Spherical gravitational model
- NRLMSISE-00 for the atmosphere
- IGRF for the geomagnetic field
- IRI for the ionosphere

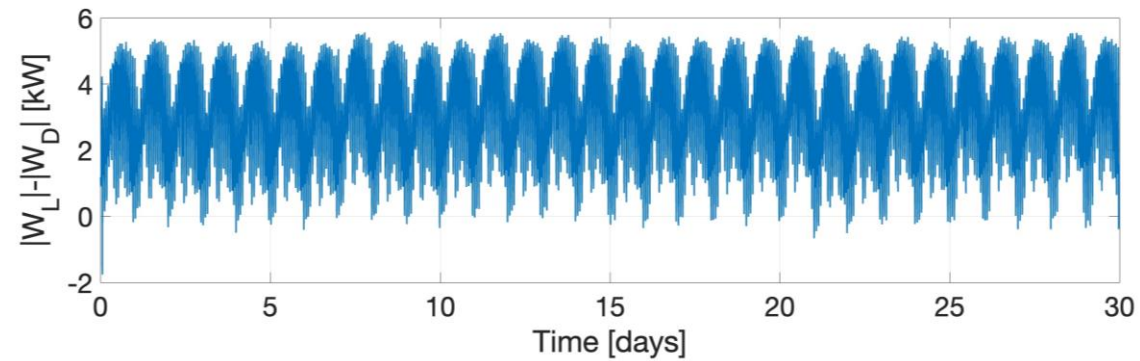
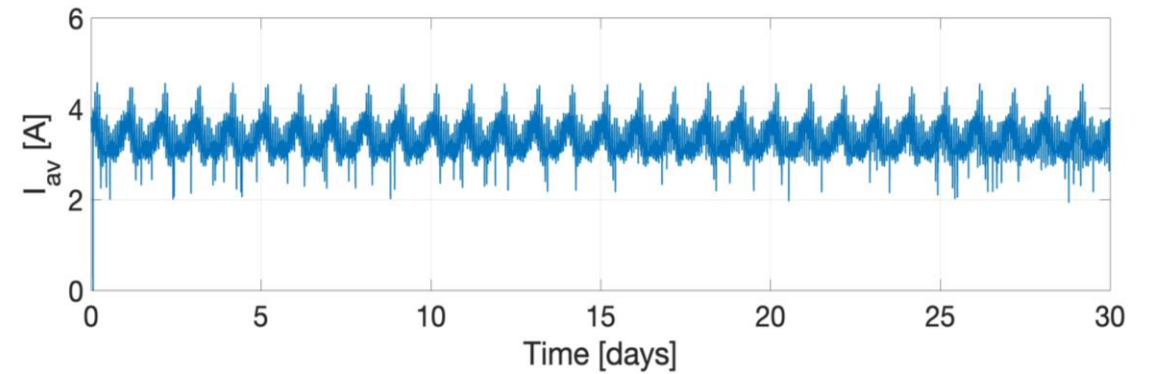
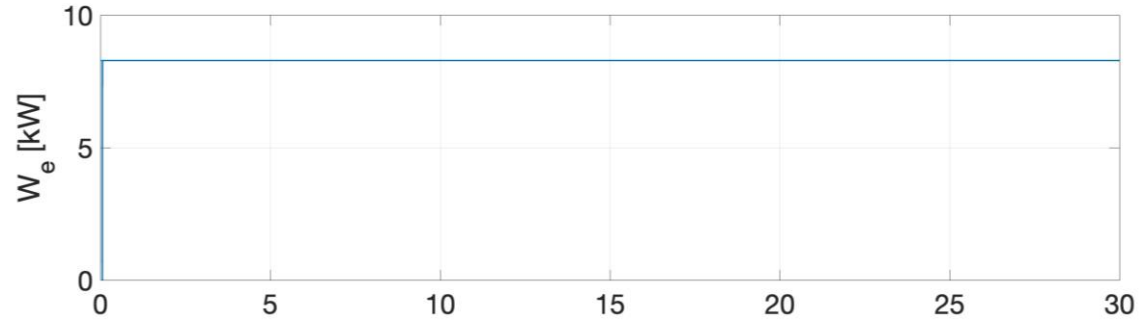
Tether is assumed to be always aligned with the local vertical.

	$F_D = 0.4 N$	$F_D = 0.8 N$
L_t	15.00 km	15.00 km
f_i	97.6%	97.0%
L_{pv}	14.64 km	14.45 km
η_{pv}	4.23 %	7.23 %

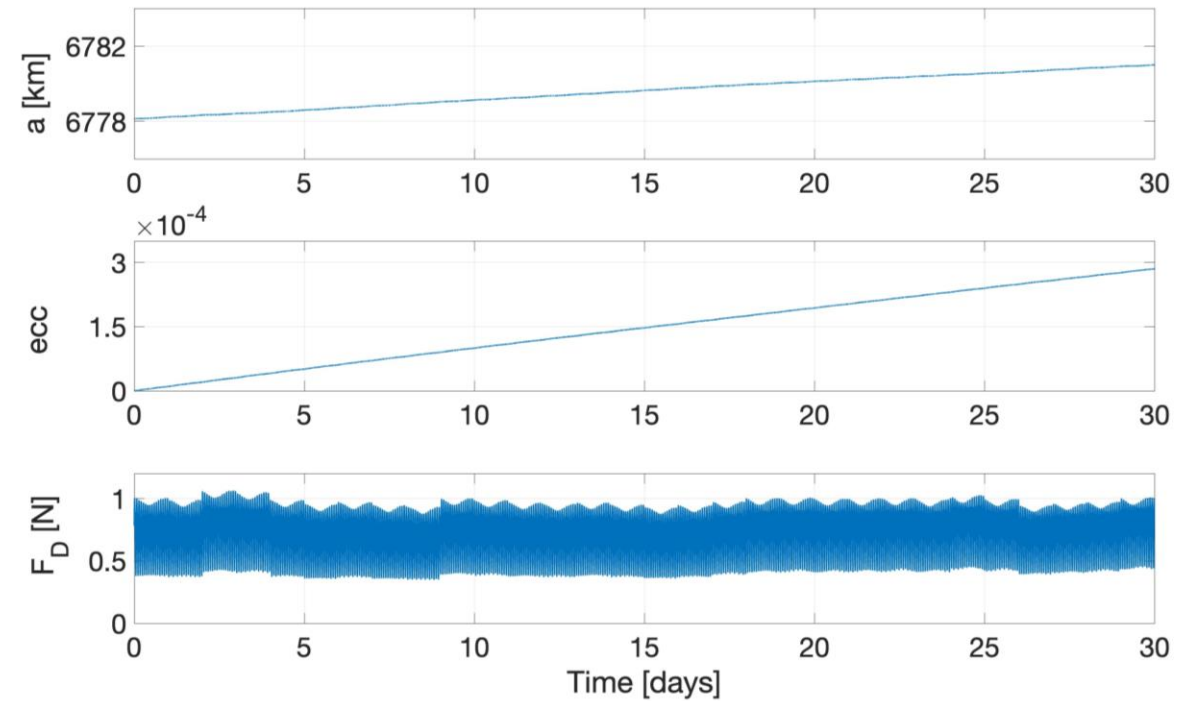
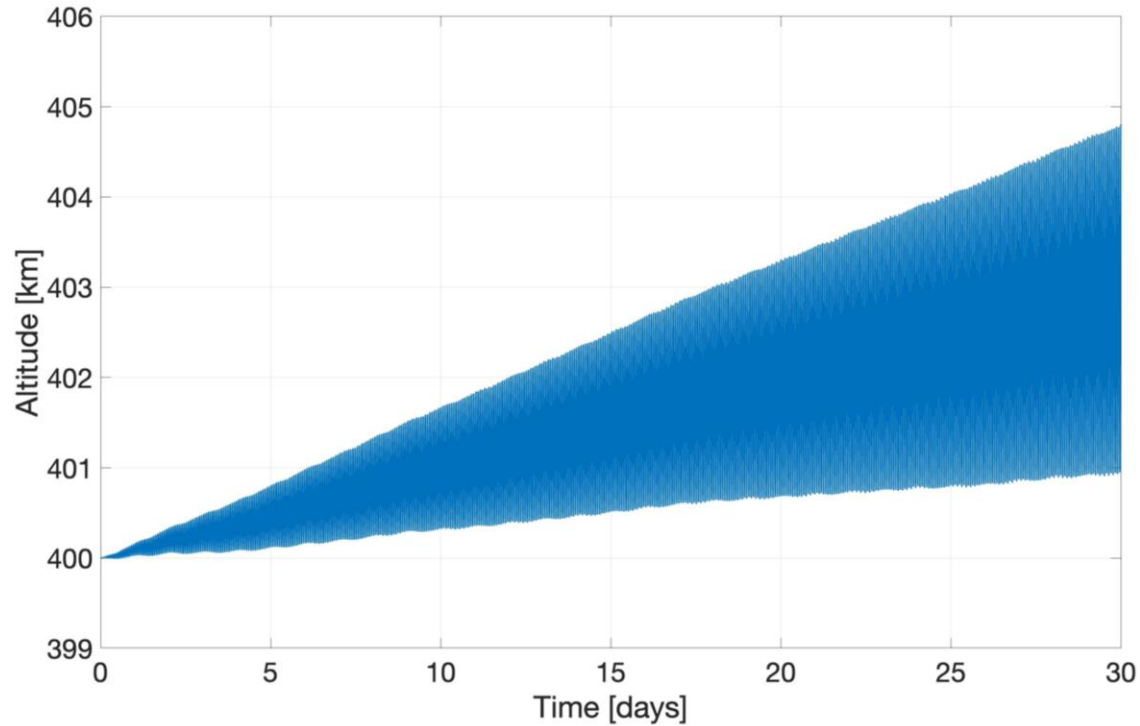




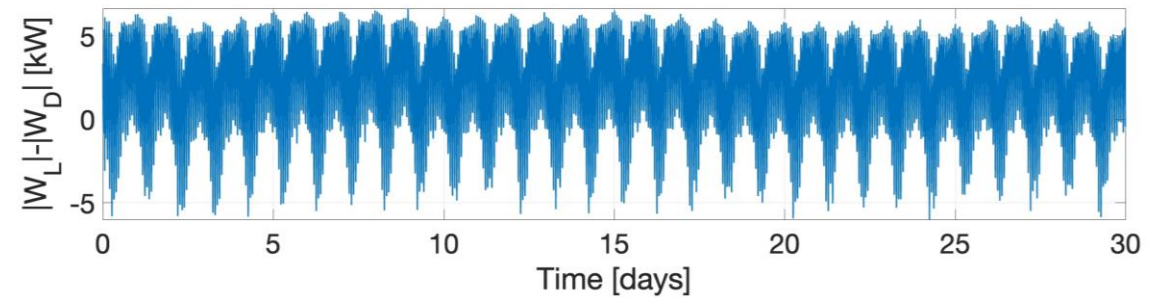
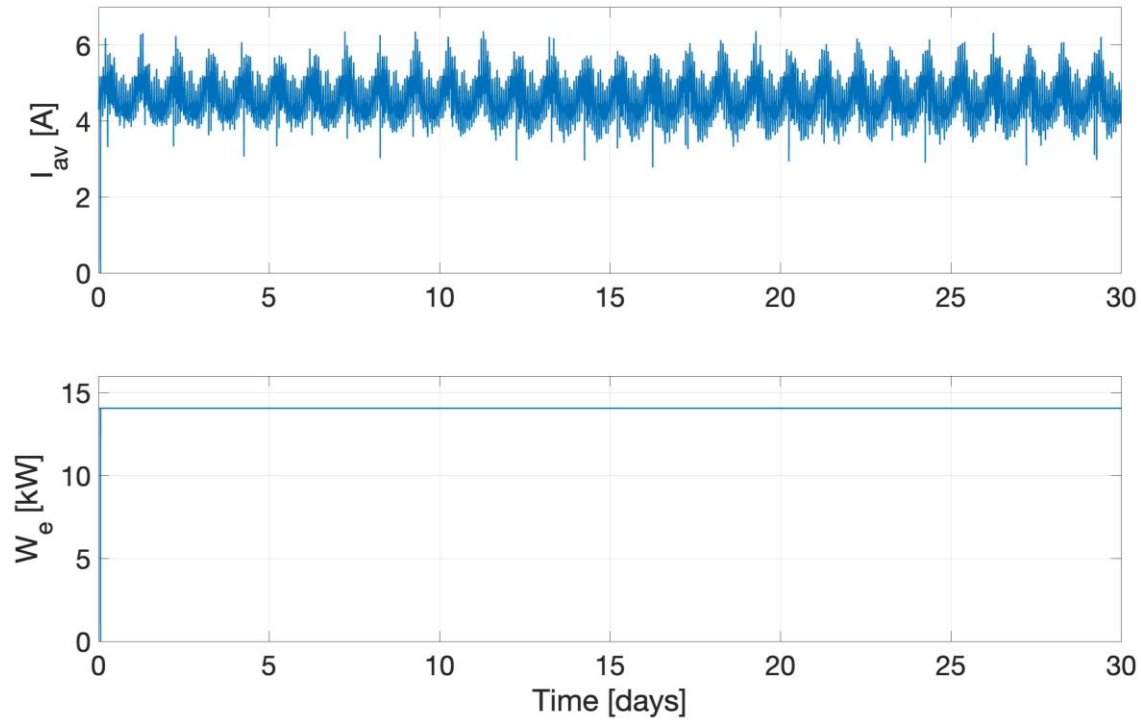
Simulation starting date is March 1st, 2003



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Simulation starting date is December 1st, 2001



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- BPT is a promising technology for the reboost of the ISS
- BPT is a fully autonomous system
- A preliminary design model was analyzed. Since the BPT should be capable of functioning effectively for several years, two options are proposed:
 - a) employing the most efficient BPT, specifically designed for the upper drag threshold
 - b) opting for a design tailored for an average drag of 0.6 N or 0.7 N
- Future investigations should be done on the stability simulating a flexible tether.

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**THANK YOU FOR THE
ATTENTION!**

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